

Technology Characterization: Steam Turbines

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Technology Characterization – Steam Turbines

Introduction and Summary

Steam turbines are one of the most versatile and oldest prime mover technologies still in general production. Power generation using steam turbines has been in use for about 100 years, when they replaced reciprocating steam engines due to their higher efficiencies and lower costs. Conventional steam turbine power plants generate most of the electricity produced in the United States. The capacity of steam turbines can range from 50 kW to several hundred MWs for large utility power plants. Steam turbines are widely used for combined heat and power (CHP) applications.

Unlike gas turbine and reciprocating engine CHP systems where heat is a byproduct of power generation, steam turbines normally generate electricity as a byproduct of heat (steam) generation. A steam turbine is captive to a separate heat source and does not directly convert fuel to electric energy. The energy is transferred from the boiler to the turbine through high-pressure steam that in turn powers the turbine and generator. This separation of functions enables steam turbines to operate with an enormous variety of fuels, from natural gas to solid waste, including all types of coal, wood, wood waste, and agricultural byproducts (sugar cane bagasse, fruit pits, and rice hulls). In CHP applications, steam at lower pressure is extracted from the steam turbine and used directly or is converted to other forms of thermal energy.

Steam turbines offer a wide array of designs and complexity to match the desired application and/or performance specifications. Steam turbines for utility service may have several pressure casings and elaborate design features, all designed to maximize the efficiency of the power plant. For industrial applications, steam turbines are generally of simpler single casing design and less complicated for reliability and cost reasons. CHP can be adapted to both utility and industrial steam turbine designs.

Applications

While steam turbines themselves are competitively priced compared to other prime movers, the costs of complete boiler/steam turbine CHP systems are relatively high on a per kW of capacity basis. This is because of their low power to heat (P/H) ratio, the costs of the boiler, fuel handling, overall steam systems, and the custom nature of most installations. Thus, steam turbines are well suited to medium- and large-scale industrial and institutional applications where inexpensive fuels, such as coal, biomass, various solid wastes and byproducts (e.g., wood chips, etc.), refinery residual oil, and refinery off gases are available. Because of the relatively high cost of the system, high annual capacity factors are required to enable a reasonable recovery of invested capital.

However, a retrofit application of steam turbines into existing boiler/steam systems is often an economic option. A turbine-generator set requires the boiler must be able to support a small increase in demand. In addition, to continue to satisfy thermal demands, the distribution system

must be able to accommodate the increased flow rate of lower-Btu steam. In such situations, the decision involves only the added capital cost of the steam turbine, its generator, controls, and electrical interconnection, with the balance of plant already in place. Similarly, many facilities faced with replacement or upgrades of existing boilers and steam systems often consider the addition of steam turbines, especially if steam requirements are relatively large compared to power needs within the facility.

In general, steam turbine applications are driven by balancing lower cost fuel or avoided disposal costs for the waste fuel, with the high capital cost and (hopefully high) annual capacity factor for the steam plant and the combined energy plant-process plant application. For these reasons, steam turbines are not normally direct competitors of gas turbines and reciprocating engines.

Industrial and CHP Applications

The primary locations of steam turbine based CHP systems is industrial processes where solid or waste fuels are readily available for boiler use. In CHP applications, steam extracted from the steam turbine directly feeds into a process or is converted to another form of thermal energy. The turbine may drive an electric generator or equipment such as boiler feedwater pumps, process pumps, air compressors, and refrigeration chillers. Turbines as industrial drivers are usually a single casing machine, either single stage or multistage, condensing or non-condensing depending on steam conditions and the value of the steam. Steam turbines operate at a single speed when driving an electric generator and operate over a speed range when driving a refrigeration compressor. For non-condensing applications, steam exhausted from the turbine is at a pressure and temperature sufficient for the CHP heating application.

There were an estimated 19,062 MW of boiler/steam turbine CHP capacity operating in the United States in 2000 located at over 580 industrial and institutional facilities. **Figure 1** shows the largest amount of capacity is in the chemicals, primary metals, and paper industries. Pulp and paper mills are often an ideal industrial/CHP application for steam turbines. Such facilities operate continuously, have a high demand for steam, and have on-site fuel supply at low, or even negative costs (waste that would have to be otherwise disposed of).

Figure 2 illustrates existing steam turbine CHP capacity by boiler fuel type. While coals fuels much of the installed boiler/steam turbine system base, large amounts of capacity are fueled by wood, waste, and a variety of other fuels.

Figure 1. Existing Boiler/Steam Turbine CHP by Industry
19,062 MW at 582 Sites

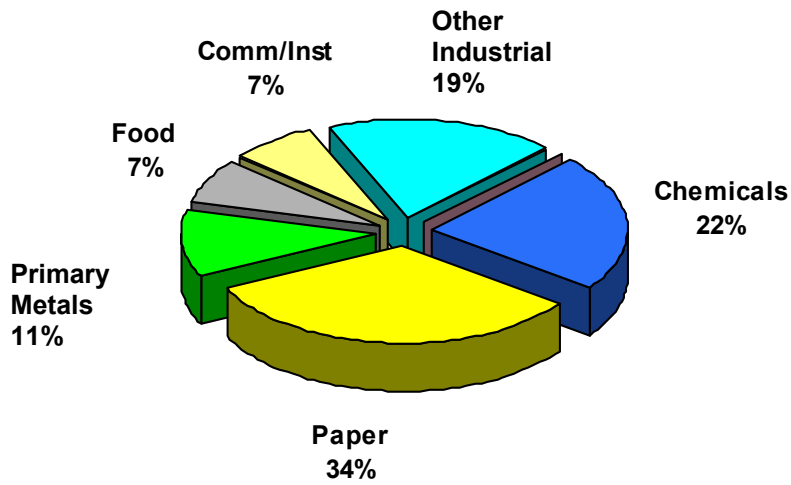
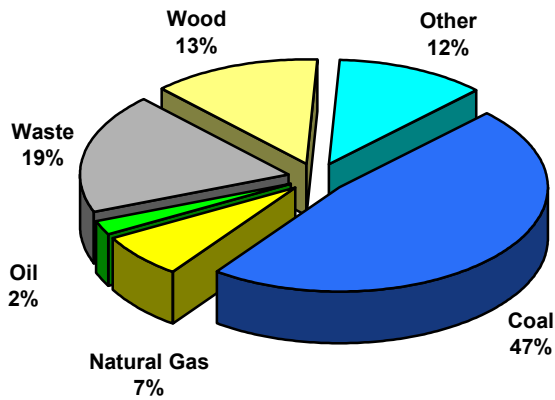


Figure 2. Existing Boiler/Steam Turbine CHP by Boiler Fuel Type
19,062 MW at 582 Sites



Source: Energy Nexus Group/Hagler Bailly.

Combined Cycle Power Plants

The trend in power plant design is the combined cycle, which incorporates a steam turbine in a bottoming cycle with a gas turbine. Steam generated in the heat recovery steam generator (HRSG) of the gas turbine is used to drive a steam turbine to yield additional electricity and improve cycle efficiency. Combined cycle CHP applications use an extraction-condensing type of steam turbine.

District Heating Systems

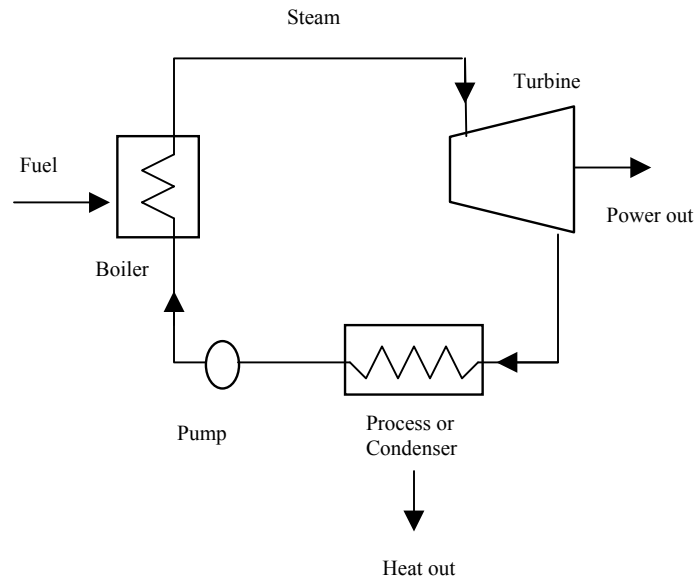
There are many cities and college campuses that have steam district heating systems where adding a steam turbine between the boiler and the distribution system may be an attractive application. Often the boiler is capable of producing moderate-pressure steam but the distribution system needs only low-pressure steam. In these cases, the steam turbine generates electricity using the higher-pressure steam, and discharges low-pressure steam into the distribution system.

Technology Description

Basic Process and Components

The thermodynamic cycle for the steam turbine is the Rankine cycle. The cycle is the basis for conventional power generating stations and consists of a heat source (boiler) that converts water to high-pressure steam. In the steam cycle, water is first pumped to medium to high pressure. It is then heated to the boiling temperature corresponding to the pressure, boiled (heated from liquid to vapor), and then most frequently superheated (heated to a temperature above that of boiling). A multistage turbine expands the pressurized steam to lower pressure and the steam is then exhausted either to a condenser at vacuum conditions or into an intermediate temperature steam distribution system that delivers the steam to the industrial or commercial application. The condensate from the condenser or from the steam utilization system returns to the feedwater pump for continuation of the cycle. **Figure 3** shows the primary components of a boiler/steam turbine system.

Figure 3. Components of a Boiler/Steam Turbine System



The steam turbine itself consists of a stationary set of blades (called nozzles) and a moving set of adjacent blades (called buckets or rotor blades) installed within a casing. The two sets of blades work together such that the steam turns the shaft of the turbine and the connected load. The stationary nozzles accelerate the steam to high velocity by expanding it to lower pressure. A rotating bladed disc changes the direction of the steam flow, thereby creating a force on the blades that, because of the wheeled geometry, manifests itself as torque on the shaft on which the bladed wheel is mounted. The combination of torque and speed is the output power of the turbine.

The internal flow passages of a steam turbine are similar to those of the expansion section of a gas turbine (indeed, gas turbine engineering came directly from steam turbine design around 100 years ago). The main differences are the different gas density, molecular weight, isentropic expansion coefficient, and to a lesser extent viscosity of the two fluids.

Compared to reciprocating steam engines of comparable size, steam turbines rotate at much higher rotational speeds, which contributes to their lower cost per unit of power developed. The absence of inlet and exhaust valves that somewhat throttle (reduce pressure without generating power) and other design features enable steam turbines to be more efficient than reciprocating steam engines. In some steam turbine designs, the blade row accomplishes part of the decrease in pressure and acceleration. These distinctions are known as impulse and reaction turbine designs, respectively. The competitive merits of these designs are the subject of business competition as both designs have sold successfully for well over 75 years.

The connection between the steam supply and the power generation is the steam, and return feedwater, lines. There are numerous options in the steam supply, pressure, temperature and extent, if any, for reheating partially expanded steam. Steam systems vary from low-pressure

lines used primarily for space heating and food preparation, to medium pressure used in industrial processes and cogeneration, to high-pressure use in utility power generation. Generally, as the system gets larger the economics favor higher pressures and temperatures with their associated heavier walled boiler tubes and more expensive alloys.

In general, utility applications involve raising steam for the exclusive purpose of power generation. Such systems also use a water-cooled condenser to exhaust the steam from the turbine at the lowest practical pressure. Some utility turbines have dual use, power generation and steam delivery at higher pressure into district heating systems or to neighboring industrial plants at pressure, and consequently do not have condensers. These plants are actually large cogeneration/CHP plants.

Boilers

Steam turbines differ from reciprocating engines and gas turbines in that the fuel is burned in a piece of equipment, the boiler, which is separate from the power generation equipment, the steam turbogenerator. As mentioned previously, this separation of functions enables steam turbines to operate with an enormous variety of fuels.

For sizes up to (approximately) 40 MW, horizontal industrial boilers are built. This enables rail car shipping, with considerable cost savings and improved quality as the cost and quality of factory labor is usually both lower in cost and greater in quality than field labor. Large shop-assembled boilers are typically capable of firing only gas or distillate oil, as there is inadequate residence time for complete combustion of most solid and residual fuels in such designs. Large, field-erected industrial boilers firing solid and residual fuels bear a resemblance to utility boilers except for the actual solid fuel injection. Large boilers usually burn pulverized coal, however intermediate and small boilers burning coal or solid fuel employ various types of solids feeders.

Types of Steam Turbines

The primary type of turbine used for central power generation is the *condensing* turbine. These power-only utility turbines exhaust directly to condensers that maintain vacuum conditions at the discharge of the turbine. An array of tubes, cooled by river, lake, or cooling tower water, condenses the steam into (liquid) water.¹ The cooling water condenses the steam turbine exhaust steam in the condenser creating the condenser vacuum. As a small amount of air leaks into the system when it is below atmospheric pressure, a relatively small compressor removes non-condensable gases from the condenser. Non-condensable gases include both air and a small amount of the corrosion byproduct of the water-iron reaction, hydrogen.

The condensing turbine processes result in maximum power and electrical generation efficiency from the steam supply and boiler fuel. The power output of condensing turbines is sensitive to ambient conditions.²

¹ At 80°F, the vapor pressure of water is 0.51 psia, at 100°F it is 0.95 psia, at 120°F it is 1.69 psia and at 140°F Fahrenheit it is 2.89 psia

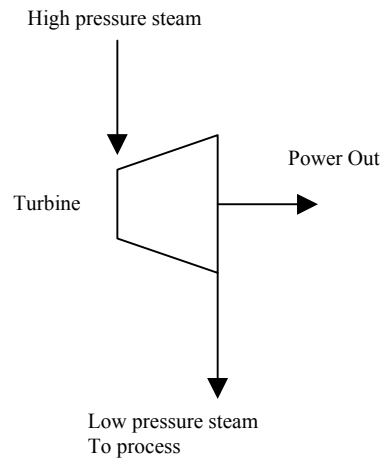
² From a reference condition of condensation at 100 degree Fahrenheit, 6.5% less power is obtained from the inlet steam when the temperature at which the steam is condensed is increased (because of higher temperature ambient conditions) to 115°F. Similarly the power output is increased by 9.5% when the condensing temperature is reduced

CHP applications use two types of steam turbines: non-condensing and extraction.

Non-Condensing (Back-pressure) Turbine

Figure 4 shows the non-condensing turbine (also referred to as a back-pressure turbine) exhausts its entire flow of steam to the industrial process or facility steam mains at conditions close to the process heat requirements.

Figure 4. Non-Condensing (Back-Pressure) Steam Turbine



Usually, the steam sent into the mains is not much above saturation temperature.³ The term “back-pressure” refers to turbines that exhaust steam at atmospheric pressures and above. The specific CHP application establishes the discharge pressure. 50, 150, and 250 psig are the most typical pressure levels for steam distribution systems. District heating systems most often use the lower pressures, and industrial processes use the higher pressures. Industrial processes often include further expansion for mechanical drives, using small steam turbines for driving heavy equipment that runs continuously for long periods. Power generation capability reduces significantly when steam is used at appreciable pressure rather than being expanded to vacuum in a condenser. Discharging steam into a steam distribution system at 150 psig can sacrifice slightly more than half the power that could be generated when the inlet steam conditions are 750 psig and 800°F, typical of small steam turbine systems.

Extraction Turbine

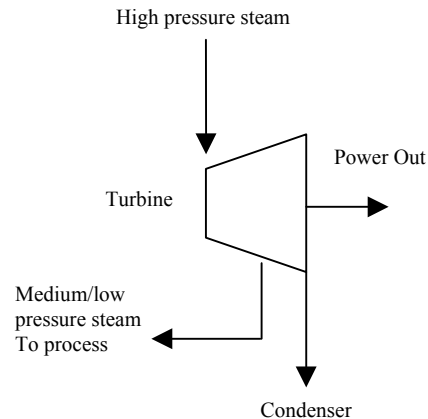
The extraction turbine has opening(s) in its casing for extraction of a portion of the steam at some intermediate pressure before condensing the remaining steam. **Figure 5** illustrates the

to 80°F. This illustrates the influence of steam turbine discharge pressure on power output and, consequently, net heat rate (and efficiency.)

³ At 50 psig (65 psia) the condensation temperature is 298°F, at 150 psig (165 psia) the condensation temperature is 366°F, and at 250 psig (265 psia) it is 406°F.

extracted steam may be used for process purposes in a CHP facility or for feedwater heating as is the case in most utility power plants.

Figure 5. Extraction Steam Turbine



The steam extraction pressure may or may not be automatically regulated. Regulated extraction permits more steam to flow through the turbine to generate additional electricity during periods of low thermal demand by the CHP system. In utility type steam turbines, there may be several extraction points, each at a different pressure corresponding to a different temperature. The facility's specific needs for steam and power over time determine the extent to which steam in an extraction turbine is extracted for use in the process.

In large, often complex, industrial plants, additional steam may be admitted (flows into the casing and increases the flow in the steam path) to the steam turbine. Often this happens when using multiple boilers at different pressure, because of their historical existence. These steam turbines are referred to as *admission* turbines. At steam extraction and admission locations there are usually steam flow control valves that add to the steam and control system cost.

Numerous mechanical design features increase efficiency, provide for operation over a range of conditions, simplify manufacture and repair, and achieve other practical purposes. The long history of steam turbine use has resulted in a large inventory of steam turbine stage designs. For example, the division of steam acceleration and change in direction of flow varies between competing turbine manufacturers under the identification of impulse and reaction designs. Manufacturers tailor clients' design requests by varying the flow area in the stages and the extent to which steam is extracted (removed from the flow path between stages) to accommodate the specification of the client.

When the steam expands through a high-pressure ratio, as in utility and large industrial steam systems, the steam can begin to condense in the turbine when the temperature of the steam drops below the saturation temperature at that pressure. If water drops form in the turbine, blade erosion occurs from the drops impact on the blades. At this point in the expansion the steam is

sometimes returned to the boiler and reheated to high temperature and then returned to the turbine for further (safe) expansion. In a few large, high pressure, utility steam systems install double reheat systems.

With these choices the designer of the steam supply system and the steam turbine have the challenge of creating a system design which delivers the (seasonally varying) power and steam which presents the most favorable business opportunity to the plant owners.

Between the power (only) output of a condensing steam turbine and the power and steam combination of a back-pressure steam turbine essentially any ratio of power to heat output can be supplied. Back-pressure steam turbines can be obtained with a variety of back pressures, further increasing the variability of the power-to-heat ratio.

Design Characteristics

| | |
|-----------------------|--|
| Custom design: | Steam turbines are designed to match CHP design pressure and temperature requirements and to maximize electric efficiency while providing the desired thermal output. |
| Thermal output: | Steam turbines are capable of operating over a broad range of steam pressures. Utility steam turbines operate with inlet steam pressures up to 3,500 psig and exhaust vacuum conditions as low as one inch of Hg (absolute). Steam turbines are custom designed to deliver the thermal requirements of the CHP applications through use of backpressure or extraction steam at appropriate pressures and temperatures. |
| Fuel flexibility: | Steam turbines offer a wide range of fuel flexibility using a variety of fuel sources in the associated boiler or other heat source, including coal, oil, natural gas, wood and waste products. |
| Reliability and life: | Steam turbine life is extremely long. When properly operated and maintained (including proper control of boiler water chemistry), steam turbines are extremely reliable, only requiring overhauls every several years. They require controlled thermal transients to minimize differential expansion of the parts as the massive casing slowly heats up. |
| Size range: | Steam turbines are available in sizes from under 100 kW to over 250 MW. In the multi-megawatt size range, industrial and utility steam turbine designations merge, with the same turbine (high-pressure section) able to serve both industrial and small utility applications. |
| Emissions: | Emissions are dependent upon the fuel used by the boiler or other steam source, boiler furnace combustion section design and operation, and built-in and add-on boiler exhaust cleanup systems. |

Performance Characteristics

Electrical Efficiency

The electrical generating efficiency of standard steam turbine power plants varies from a high of 37% HHV⁴ for large, electric utility plants designed for the highest practical annual capacity factor, to under 10% HHV for small, simple plants which make electricity as a byproduct of delivering steam to processes or district heating systems.

Steam turbine thermodynamic efficiency (isentropic efficiency) refers to the ratio of power actually generated from the turbine to what would be generated by a perfect turbine with no internal losses using steam at the same inlet conditions and discharging to the same downstream pressure (actual enthalpy drop divided by the isentropic enthalpy drop). Turbine thermodynamic efficiency is not to be confused with electrical generating efficiency, which is the ratio of net power generated to total fuel input to the cycle. Steam turbine thermodynamic efficiency measures how efficiently the turbine extracts power from the steam itself. Multistage (moderate to high-pressure ratio) steam turbines have thermodynamic efficiencies that vary from 65% for small (under 1,000 kW) units to over 90% for large industrial and utility sized units. Small, single stage steam turbines can have efficiencies as low as 50%. When a steam turbine exhausts to a CHP application, the turbine efficiency is not as critical as in a power only condensing mode. The majority of the energy not extracted by the steam turbine satisfies the thermal load. Power only applications waste the exhaust turbine steam energy in condensers.

Table 1 summarizes performance characteristics for typical commercially available steam turbines and for typical boiler/steam CHP systems in the 500 kW to 15 MW size range.

⁴ All turbine and engine manufacturers quote heat rates in terms of the lower heating value (LHV) of the fuel. However, the usable energy content of fuels is typically measured on a higher heating value basis (HHV). In addition, electric utilities measure power plant heat rates in terms of HHV. For natural gas, the average heat content of natural gas is 1,030 Btu/scf on an HHV basis and 930 Btu/scf on an LHV basis – or about a 10% difference.

Table 1. Boiler/Steam Turbine CHP System Cost and Performance Characteristics*

| Cost & Performance Characteristics ⁵ | System 1 | System 2 | System 3 |
|--|---------------|---------------|---------------|
| Steam Turbine Parameters | | | |
| Nominal Electricity Capacity (kW) | 500 | 3,000 | 15,000 |
| Turbine Type | Back Pressure | Back Pressure | Back Pressure |
| Equipment Cost (\$/kW) ⁶ | 540 | 225 | 205 |
| Total Installed Cost (\$/kW) ⁷ | 918 | 385 | 349 |
| Turbine Isentropic Efficiency (%) ⁸ | 50% | 70% | 80% |
| Generator/Gearbox Efficiency (%) | 94% | 94% | 97% |
| Steam Flow (lbs/hr) | 21,500 | 126,000 | 450,000 |
| Inlet Pressure (psig) | 500 | 600 | 700 |
| Inlet Temperature (° Fahrenheit) | 550 | 575 | 650 |
| Outlet Pressure (psig) | 50 | 150 | 150 |
| Outlet Temperature (° Fahrenheit) | 298 | 366 | 366 |
| CHP System Parameters | | | |
| Boiler Efficiency (%), HHV | 80% | 80% | 80% |
| CHP Electric Efficiency (%), HHV ⁹ | 6.4% | 6.9% | 9.3% |
| Fuel Input (MMBtu/hr) ¹⁰ | 26.7 | 147.4 | 549.0 |
| Steam to Process (MMBtu/hr) | 19.6 | 107.0 | 386.6 |
| Steam to Process (kW) | 5,740 | 31,352 | 113,291 |
| Total CHP Efficiency (%), HHV ¹¹ | 79.6% | 79.5% | 79.7% |
| Power/Heat Ratio ¹² | 0.09 | 0.10 | 0.13 |
| Net Heat Rate (Btu/kWh) ¹³ | 4,515 | 4,568 | 4,388 |
| Effective Electrical Efficiency (%), HHV ¹⁴ | 75.6% | 75.1% | 77.8% |

* For typical systems commercially available in 2002

⁵ Characteristics for “typical” commercially available steam turbine generator systems. Steam turbine data based on information from: TurboSteam, Inc for 500 kW and 3 MW; General Electric for 15 MW turbine.

⁶ Equipment cost includes turbine, gearbox, generator, controls, and switchgear; boiler and steam system costs are not included.

⁷ Installed costs vary greatly based on site-specific conditions; Installation costs of a “typical” simple installation were estimated to be 70% of the equipment costs.

⁸ The Isentropic efficiency of a turbine is a comparison of the actual power output compared to the ideal, or isentropic, output. It is a measure of the effectiveness of extracting work from the expansion process and is used to determine the outlet conditions of the steam from the turbine.

⁹ CHP electrical efficiency = Net electricity generated/Total fuel into boiler; A measure of the amount of boiler fuel converted into electricity.

¹⁰ Fuel input based on condensate return at steam outlet pressure and saturation temperature.

¹¹ Total CHP efficiency = (Net electricity generated+Net steam to process)/Total fuel into boiler

¹² Power/Heat Ratio = CHP electrical power output (Btu)/ useful heat output (Btu)

¹³ Net Heat Rate = (total fuel input to the boiler - the fuel that would required to generate the steam to process assuming the same boiler efficiency/steam turbine electric output (kW).

¹⁴ Effective Electrical Efficiency = (Steam turbine electric power output)/(Total fuel into boiler – (steam to process/boiler efficiency)). Equivalent to 3,412 Btu/kWh/Net Heat Rate.

Operating Characteristics

Steam turbines, especially smaller units, leak steam around blade rows and out the end seals. When an end is at a low pressure, as is the case with condensing steam turbines, air can also leak into the system. The leakages cause less power to be produced than expected, and the makeup water has to be treated to avoid boiler and turbine material problems. Air that has leaked in needs to be removed, which is usually done by a compressor removing non-condensable gases from the condenser.

Because of the high pressures used in steam turbines, the casing is quite thick, and consequently steam turbines exhibit large thermal inertia. Steam turbines must be warmed up and cooled down slowly to minimize the differential expansion between the rotating blades and the stationary parts. Large steam turbines can take over ten hours to warm up. While smaller units have more rapid startup times, steam turbines differ appreciably from reciprocating engines, which start up rapidly, and from gas turbines, which can start up in a moderate amount of time and load follow with reasonable rapidity. Steam turbine applications usually operate continuously for extended periods, although the steam fed to the unit and the power delivered may vary (slowly) during such periods of continuous operation.

Process Steam and Performance Tradeoffs

The amount and quality of recovered heat is a function of the entering steam conditions and the design of the steam turbine. Exhaust steam from the turbine is used directly in a process or is converted to other forms of thermal energy, including hot or chilled water. Steam discharged or extracted from a steam turbine can be used in a single- or double effect absorption chiller. The steam turbine can also be used as a mechanical drive for a centrifugal chiller.

CHP System Efficiency

Steam turbine CHP systems generally have low power to heat ratios, typically in the 0.05 to 0.2 range. This is because electricity is a byproduct of heat generation, with the system optimized for steam production. Hence, while steam turbine CHP system electrical efficiency¹⁵ may seem low, it is because the primary objective is to produce large amounts of steam. The effective electrical efficiency¹⁶ of steam turbine systems, however, is generally high, because almost all the energy difference between the high-pressure boiler output and the lower pressure turbine output is converted to electricity. This means that total CHP system efficiencies¹⁷ are generally high and approach the boiler efficiency level. Steam boiler efficiencies range from 70 to 85 % HHV depending on boiler type and age, fuel, duty cycle, application, and steam conditions.

Performance and Efficiency Enhancements

In industrial steam turbine systems, business conditions determine the requirements and relative values of electric power and steam. Plant system engineers then decide the extent of efficiency

¹⁵ Net power output / total fuel input into the system.

¹⁶ (Steam turbine electric power output)/(Total fuel into boiler – (steam to process/boiler efficiency)).

¹⁷ Net power and steam generated divided by total fuel input.

enhancing options to incorporate in terms of their incremental effects on performance and plant cost, and select appropriate steam turbine inlet and exhaust conditions. Often the steam turbine is going into a system that already exists and is being modified, so that a number of steam system design parameters are already determined by previous decisions, which exist as system hardware characteristics.

As the stack temperature of the boiler exhaust combustion products still contain some heat, tradeoffs occur regarding the extent of investment in heat reclamation equipment for the sake of efficiency improvement. Often the stack exhaust temperature is set at a level where further heat recovery would result in condensation of corrosive chemical species in the stack, with consequential deleterious effects on stack life and safety.

Steam Reheat

Higher pressures and steam reheat increase power generation efficiency in large industrial (and utility) systems. The higher the pressure ratio (the ratio of the steam inlet pressure to the steam exit pressure) across the steam turbine, and the higher the steam inlet temperature, the more power it will produce per unit of mass flow. To avoid condensation the inlet steam temperature is increased to the economic practical limit of materials. This limit is now generally in the range of 800 to 900°F for small industrial steam turbines.

When the economically practical limit of temperature is reached, the expanding steam can reach a condition of temperature and pressure where condensation to (liquid) water begins. Small amounts of water droplets can be tolerated in the last stage of a steam turbine provided that the droplets are not too large or numerous. At pressures higher than that point the steam is returned to the boiler and reheated in temperature and then returned to the expansion steam turbine for further expansion. When returned to the next stage of the turbine, the steam expands without condensation.

Combustion Air Preheating

In large industrial systems, air preheaters recover heat from the boiler exhaust gas stream, and use it to preheat the combustion air, thereby reducing fuel consumption. Boiler combustion air preheaters are large versions of the heat wheels used for the same purpose on industrial furnaces.

Capital Cost

A steam turbine-based CHP plant is a complex process with many interrelated subsystems that must be usually be custom designed. A typical breakdown of installed costs for a steam turbine CHP plant is 25% - boiler, 25% - fuel handling, storage and preparation system, 20% - stack gas cleanup and pollution controls, 15% steam turbine generator, and 20% - field construction and plant engineering. Boiler costs are highly competitive. Typically, the only area in which significant cost reductions can be made when designing a system is in fuel handling/storage/preparation.

In a steam turbine cogeneration plant, especially one burning solid fuel such as biomass, the turbine accounts for a much smaller portion of total system installed costs than is the case with internal combustion engines and industrial gas turbines. Often the solid fuel-handling equipment alone costs as much as 90% of the cost of the steam turbine. The pollution control and

electrostatic precipitator cost can reach 80% of the steam turbine cost. A typical coal/wood fired boiler costs more than the steam turbine.¹⁸ The cost of complete solid fuel cogeneration plants varies with many factors, with fuels handling, pollution control equipment and boiler cost all being major cost items. Because of both the size of such plants and the diverse sources of the components, solid fuel cogeneration plants invariably involve extensive system engineering and field labor during construction. Typical complete plant costs run well over \$1,000/kW, with little generalization except that for the same fuel and configuration, costs per kW of capacity generally increase as size decreases.

Steam turbine costs exhibit a modest extent of irregularity, as steam turbines are made in sizes with finite steps between the sizes. The cost of the turbine is generally the same for the upper and lower limit of the steam flowing through it, so step-like behavior is sometimes seen in steam turbine prices. Since they come in specific size increments, a steam turbine that is used at the upper end of its range of power capability costs less per kW generated than one that is used at the lower end of its capability.

Often steam turbines are sold to fit into an existing plant. In some of these applications, the specifications, mass flow, pressure, temperature and backpressure or extraction conditions are not conditions for which large competition exists. These somewhat unique machines are more expensive per kilowatt than are machines for which greater competition exists, for three reasons: 1) a greater amount of custom engineering and manufacturing setup may be required; 2) there is less potential for sales of duplicate or similar units; and 3) there are fewer competitive bidders. The truly competitive products are the “off-the-rack” type machines, while “custom” machines are naturally more expensive.

Steam turbine prices vary greatly with the extent of competition and related manufacturing volumes for units of desired size, inlet and exit steam conditions, rotational speed and standardization of construction. Quoted prices are usually for an assembled steam turbine-electrical generator package. The electrical generator can account for 20% to 40% of the assembly. As the steam turbine/electrical generator package is heavy, due in large part to the heavy walled construction of the high-pressure turbine casing, it requires careful mounting on an appropriate pedestal. The installation and connection to the boiler through high pressure-high temperature steam pipes require engineering and installation expertise. As the high-pressure steam pipes typically vary in temperature by 750°F between cold standby/repair status and full power status, care must be taken in installing a means to accommodate the differential expansion accompanying startup and shutdown. Should the turbine have variable extraction, the cost of the extraction valve and control system adds to the installation.

Small sized steam turbines, below about 2 MW, have a relatively small market, as complete plant cost becomes high enough so that the business venture has much less attractiveness. In these small sizes there is less competition and lower manufacturing volume, so that component costs are not as competitive, the economies of scale in both size and manufacturing volumes disfavor

¹⁸ Spiewak and Weiss, loc. Cit., pages 82 and 95. These figures are for a 32.3 MW multi-fuel fired, 1,250 psig, 900 °F, 50 psig backpressure steam turbine used in an industrial cogeneration plant

such small sizes, and the fraction of total cost due to system engineering and field construction are high.¹⁹

Boiler combustion produces the steam for a steam turbine and the temperature of the steam is limited by furnace heat transfer design, manufacturing consideration, and boiler tube bundle design. Higher heat fluxes in the boiler enable more compact boilers, with less boiler tube material to be built; however, higher heat fluxes also result in higher boiler tube temperature and the need for the use of a higher grade (adequate strength at higher temperature) boiler tube material. Such engineering economic tradeoffs between temperature (with consequential increases in efficiency) and cost appear throughout the steam plant.

Because of the temperature limitation on boiler tubes, which are exposed to the high temperature and heat flux in the furnace, steam turbine material selection is easier. An often-overlooked component in the steam power system is the steam (safety) stop valve, which is immediately ahead of the steam turbine and is designed to be able to experience the full temperature and pressure of the steam supply. This safety valve is necessary because if the generator electric load were lost (an occasional occurrence), the turbine would rapidly overspeed and destroy itself. Other accidents are possible, supporting the need for the turbine stop valve, which adds significant cost to the system

Maintenance

Steam turbines are rugged units, with operational life often exceeding 50 years. Maintenance is simple, comprised mainly of making sure that all fluids (steam flowing through the turbine and the oil for the bearing) are always clean and at the proper temperature. The oil lubrication system must be clean and at the correct operating temperature and level to maintain proper performance. Other items include inspecting auxiliaries such as lubricating-oil pumps, coolers and oil strainers and checking safety devices such as the operation of overspeed trips.

In order to obtain reliable service, steam turbines require long warmup periods so that there are minimal thermal expansion stresses and wear concerns. Steam turbine maintenance costs are quite low, typically less than \$0.004 per kWh. Boilers and any associated solid fuel processing and handling equipment that is part of the boiler/steam turbine plant require their own types of maintenance.

One maintenance issue with steam turbines is solids carry over from the boiler that deposit on turbine nozzles and other internal parts and degrades turbine efficiency and power output. Some of these are water soluble but others are not. Three methods are employed to remove such deposits: 1) manual removal; 2) cracking off deposits by shutting the turbine off and allowing it to cool; and 3) for water soluble deposits, water washing while the turbine is running.

¹⁹ Data on steam generator costs shows cost increasing with decreasing size, with a 5.25 MW, 900 psig, 850°F, 125 psig backpressure steam turbine/generator costing \$285/kW (installed). In that installation the boiler alone, excluding fuel handling and pollution control equipment, cost 150% of the cost of the steam turbine.

Fuels

Industrial boilers operate on a variety of fuels, including wood, coal, natural gas, oils (including residual oil), municipal solid waste, and sludges. The fuel handling, storage, and preparation equipment needed for solid fuels add considerably to the cost of an installation. Thus, such fuels are used only when a high annual capacity factor is expected of the facility, or when the solid material has to be disposed of to avoid an environmental or space occupancy problem.

Availability

Steam turbines generally have 99% plus availability with longer than one year between shutdowns for maintenance and inspections. This high level of availability applies only to the steam turbine, not the boiler or HRSG that is supplying the steam.

Emissions

Emissions associated with a steam turbine are dependent on the source of the steam. Steam turbines can be used with a boiler firing any one or a combination of a large variety of fuel sources, or they can be used with a gas turbine in a combined cycle configuration. Boiler emissions vary depending on fuel type and environmental conditions. Boilers emissions include nitrogen oxide (NO_x), sulfur oxides (SO_x), particulate matter (PM), carbon monoxide (CO), and carbon dioxide (CO_2).

Nitrogen Oxides (NO_x)

The pollutant referred to as NO_x is a mixture of (mostly) nitric oxide (NO) and nitrogen dioxide (NO_2) in variable composition. NO_x forms by three mechanisms: thermal NO_x , prompt NO_x , and fuel-bound NO_x . In industrial boilers, thermal and fuel-bound are the predominant NO_x formation mechanisms. Thermal NO_x , formed when nitrogen and oxygen in the combustion air combine in the flame, comprises the majority of NO_x formed during the combustion of gases and light oils. Fuel-bound NO_x is associated with oil fuels and forms when nitrogen in the fuel and oxygen in the combustion air react.

The most significant factors influencing the level of NO_x emissions from a boiler are the flame temperature and the amount of nitrogen in the fuel. Other factors include excess air level and combustion air temperature.

Sulfur Compounds (SO_x)

Emissions of sulfur relate directly to the sulfur content of the fuel, and are not dependent on boiler size or burner design. Sulfur dioxide (SO_2) composes about 95% of the emitted sulfur and with the remaining 5% emitted as sulfur trioxide (SO_3). SO_x are pollutants because they react with water vapor and form sulfuric acid mist, which is extremely corrosive and damaging in its air-, water- and soil-borne forms. Boiler fuels containing sulfur are primarily coal, oil, and some types of waste.

Particulate Matter (PM)

PM emissions are largely dependent on the grade of boiler fuel, and consist of many different compounds, including nitrates, sulfates, carbons, oxides and other uncombusted fuel elements. PM levels from natural gas are significantly lower than those of oils, and distillate oils much

lower than residual oils. For industrial and commercial boilers, the most effective method of PM control is use of higher-grade fuel, and ensuring proper burner setup, adjustment and maintenance.

Carbon Monoxide (CO)

CO forms during combustion when carbon in the fuel oxidizes incompletely, ending up as CO instead of CO₂. Older boilers generally have higher levels of CO than new equipment because older burner designs do not have CO controls. Poor burner design or firing conditions are responsible for high levels of CO boiler emissions. Proper burner maintenance or equipment upgrades, or using an oxygen control package, can control CO emissions successfully.

Carbon Dioxide (CO₂)

While not considered a regulated pollutant in the ordinary sense of directly affecting public health, emissions of carbon dioxide are of concern due to its contribution to global warming. Atmospheric warming occurs because solar radiation readily penetrates to the surface of the planet but infrared (thermal) radiation from the surface is absorbed by the CO₂ (and other polyatomic gases such as water vapor, methane, unburned hydrocarbons, refrigerants and volatile chemicals) in the atmosphere, with resultant increase in temperature of the atmosphere. The amount of CO₂ emitted is a function of both fuel carbon content and system efficiency. The fuel carbon content of natural gas is 34 lbs carbon/MMBtu; oil is 48 lbs carbon/MMBtu; and (ash-free) coal is 66 lbs carbon/MMBtu.

Typical Emissions

Table 2 below illustrates typical emissions of NO_x, PM and CO for boilers by size of steam turbine system and by fuel type.

Table 2. Typical Boiler Emissions Ranges

| Boiler Fuel | System 1 500 kW | | | Systems 2 and 3 3 MW / 15 MW | | |
|----------------------------|--------------------|------|-----------|---------------------------------|----------|-----------|
| | NO _x | CO | PM | NO _x | CO | PM |
| Coal (lbs/MMBtu) | N/A | N/A | N/A | 0.20-1.24 | 0.02-0.7 | |
| Wood (lbs/MMBtu) | 0.22-0.49 | 0.6 | 0.33-0.56 | 0.22-0.49 | 0.06 | 0.33-0.56 |
| Fuel Oil (lbs/MMBtu) | 0.15-0.37 | 0.03 | 0.01-0.08 | 0.07-0.31 | 0.03 | 0.01-0.08 |
| Natural Gas (lbs/MMBtu) | 0.03-0.1 | 0.08 | - | 0.1 – 0.28 | 0.08 | - |

Note: all emissions values are without post-combustion treatment.

Source: EPA, *Compilation of Air Pollutant Emission Factors, AP-42, Fifth Edition, Volume I: Stationary Point and Area Sources*

Boiler Emissions Control Options - NO_x

NO_x control has been the primary focus of emission control research and development in boilers. The following provides a description of the most prominent emission control approaches.

Combustion Process Emissions Control

Combustion control techniques are less costly than post-combustion control methods and are often used on industrial boilers for NO_x control. Control of combustion temperature has been the principal focus of combustion process control in boilers. Combustion control requires tradeoffs – high temperatures favor complete burn up of the fuel and low residual hydrocarbons and CO, but promote NO_x formation. Lean combustion dilutes the combustion process and reduces combustion temperatures and NO_x formation, and allows a higher compression ratio or peak firing pressures resulting in higher efficiency. However, if the mixture is too lean, misfiring and incomplete combustion occurs, increasing CO and VOC emissions.

Flue Gas Recirculation (FGR)

FGR is the most effective technique for reducing NO_x emissions from industrial boilers with inputs below 100 MMBtu/hr. With FGR, a portion of the relatively cool boiler exhaust gases re-enter the combustion process, reducing the flame temperature and associated thermal NO_x formation. It is the most popular and effective NO_x reduction method for firetube and watertube boilers, and many applications can rely solely on FGR to meet environmental standards.

External FGR employs a fan to recirculate the flue gases into the flame, with external piping carrying the gases from the stack to the burner. A valve responding to boiler input controls the recirculation rate. Induced FGR relies on the combustion air fan for flue gas recirculation. A portion of the gases travel via ductwork or internally to the air fan, where they are premixed with combustion air and introduced into the flame through the burner. Induced FGR in newer designs uses an integral design that is relatively uncomplicated and reliable. The physical limit to NO_x reduction via FGR is 80% in natural gas-fired boilers and 25% for standard fuel oils.

Low Excess Air Firing (LAE)

Excess air ensures complete combustion. However, excess air levels greater than 45% can result in increased NO_x formation, because the excess nitrogen and oxygen in the combustion air entering the flame combine to form thermal NO_x. Firing with low excess air means limiting the amount of excess air that enters the combustion process, thus limiting the amount of extra nitrogen and oxygen entering the flame. Burner design modification accomplishes this and optimization uses oxygen trim controls. LAE typically results in overall NO_x reductions of 5 to 10% when firing with natural gas, and is suitable for most boilers.

Low Nitrogen Fuel Oil

NO_x formed by fuel-bound nitrogen can account for 20 to 50% of total NO_x levels in oil-fired boiler emissions. The use of low nitrogen fuels in boilers firing distillate oils is one method of reducing NO_x emissions. Such fuels can contain up to 20 times less fuel-bound nitrogen than

standard No. 2 oil. NO_x reductions of up to 70% over NO_x emissions from standard No. 2 oils have been achieved in firetube boilers utilizing flue gas recirculation.

Burner Modifications

Modifying the design of standard burners to create a larger flame achieves lower flame temperatures and results in lower thermal NO_x formation. While most boiler types and sizes can accommodate burner modifications, it is most effective for boilers firing natural gas and distillate fuel oils, with little effectiveness in heavy oil-fired boilers. Also, burner modifications must be complemented with other NO_x reduction methods, such as flue gas recirculation, to comply with the more stringent environmental regulations. Achieving low NO_x levels (30 ppm) through burner modification alone can adversely impact boiler operating parameters such as turndown, capacity, CO levels, and efficiency.

Water/Steam Injection

Injecting water or steam into the flame reduces flame temperature, lowering thermal NO_x formation and overall NO_x emissions. However, under normal operating conditions, water/steam injection can lower boiler efficiency by 3 to 10%. Also, there is a practical limit to the amount that can be injected without causing condensation-related problems. This method is often employed in conjunction with other NO_x control techniques such as burner modifications or flue gas recirculation. When used with natural gas-fired boilers, water/steam injection can result in NO_x reduction of up to 80%, with lower reductions achievable in oil-fired boilers.

Post-Combustion Emissions Control

There are several types of exhaust gas treatment processes that are applicable to industrial boilers.

Selective Non-Catalytic Reduction (SNCR)

In boiler SNCR, a NO_x reducing agent such as ammonia or urea is injected into the boiler exhaust gases at a temperature in the 1,400 to 1,600°F range. The agent breaks down the NO_x in the exhaust gases into water and atmospheric nitrogen (N₂). While SNCR can reduce boiler NO_x emissions by up to 70%, it is difficult to apply to industrial boilers that modulate or cycle frequently because to perform properly, the agent must be introduced at a specific flue gas temperature. The location of the exhaust gases at the necessary temperature is constantly changing in a cycling boiler.

Selective Catalytic Reduction (SCR)

This technology involves the injection of the reducing agent into the boiler exhaust gas in the presence of a catalyst. The catalyst allows the reducing agent to operate at lower exhaust temperatures than SNCR, in the 500 to 1,200°F depending on the type of catalyst. NO_x reductions of up to 90% are achievable with SCR. The two agents used commercially are ammonia (NH₃ in anhydrous liquid form or aqueous solution) and aqueous urea. Urea decomposes in the hot exhaust gas and SCR reactor, releasing ammonia. Approximately 0.9 to 1.0 moles of ammonia is required per mole of NO_x at the SCR reactor inlet in order to achieve an 80 to 90% NO_x reduction.

SCR is however costly to use and can only occasionally be justified on boilers with inputs of less than 100 MMBtu/hr. SCR requires on-site storage of ammonia, a hazardous chemical. In addition, ammonia can “slip” through the process unreacted, contributing to environmental health concerns.

Boiler Emissions Control Options - SO_x

The traditional method for controlling SO_x emissions is dispersion via a tall stack to limit ground level emissions. The more stringent SO_x emissions requirements in force today demand the use of reduction methods as well. These include use of low sulfur fuel, desulfurizing fuel, and flue gas desulfurization (FGD). Desulfurization of fuel primarily applies to coal, and, like FGD, is principally used for utility boiler emissions control. Use of low sulfur fuels is the most cost effective SO_x control method for industrial boilers, as it does not require installation and maintenance of special equipment.

FGD systems are of two types: non-regenerable and regenerable. The most common, non-regenerable, results in a waste product that requires proper disposal. Regenerable FGD converts the waste product into a product that is saleable, such as sulfur or sulfuric acid. FGD reduces SO_x emissions by up to 95%.